

# Hybrid dimensional two phase flows in fractured porous media

Roland Masson

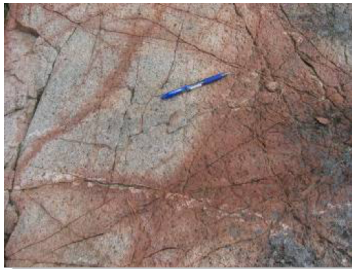
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- Modelling Darcy flows in Discrete Fracture Networks
- The Vertex Approximate Gradient Discretization (VAG)
- Applications and Numerical Results

# Fractured porous media: multiple scales (figures from J. R. de Dreuzy, Geosciences Rennes and team INRIA Sage)



# Fractured porous media: applications

- Oil and gas exploration and production
- Hydrogeology
- Geothermal energy
- Geological storages
- Soil remediation
- ...

# Flow in Fractured porous media: two main approaches

- **Double Continuum Media**: 3D fracture medium coupled to 3D matrix medium
- **Discrete fracture models (DFM)**: 2D fracture model coupled to 3D matrix medium
- Possibility to couple both approaches
  - Double Continuum media for small fractures coupled with DFM for large fractures
  - Numerical Homogenization: parameters of the Double Continuum media computed by a DFM model

# Modelling Darcy flows in Discrete Fracture Networks

# Equi-dimensional model in phase pressures formulation

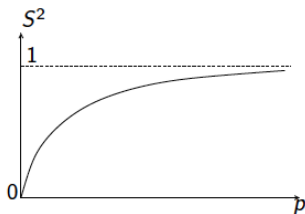
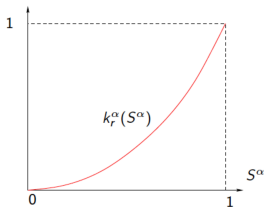
$u^\alpha$  : phase pressure

$\alpha = 1$  : wetting phase,  $\alpha = 2$  : non wetting phase

$p = u^2 - u^1$  : capillary pressure

$S^2(\mathbf{x}, p)$  : inverse of capillary pressure graph,  $S^1(\mathbf{x}, p) = 1 - S^2(\mathbf{x}, p)$

$k^\alpha(\mathbf{x}, S^\alpha) = \frac{k_r^\alpha(\mathbf{x}, S^\alpha)}{\mu^\alpha}$  : phase mobility



# Equi-dimensional model in phase pressures formulation

- Rock properties:
  - $\phi(\mathbf{x})$  : porosity
  - $\Lambda(\mathbf{x})$  : absolute permeability
- Fluid model:
  - Incompressible flow (fixed densities  $\rho^\alpha$ ,  $\alpha = 1, 2$ ),
  - Immiscible flow

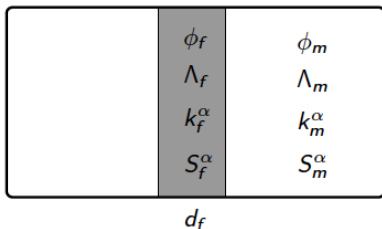
## Darcy velocities:

$$\mathbf{q}^\alpha = -k^\alpha(\mathbf{x}, S^\alpha(\mathbf{x}, p)) \Lambda(\mathbf{x})(\nabla u^\alpha - \rho^\alpha \mathbf{g}), \quad \alpha = 1, 2,$$

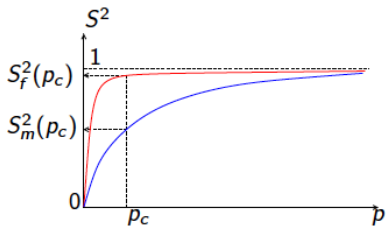
## Volume conservation for each phase:

$$\phi(\mathbf{x})\partial_t S^\alpha(\mathbf{x}, p) + \operatorname{div}(\mathbf{q}^\alpha) = 0, \quad \alpha = 1, 2.$$

# Equi-dimensional model: matrix and fracture domains



- Fracture: can act as drain or barrier
- Fracture width:  $d_f \ll$  matrix size  $L$
- Fracture rocktype (f):  $\Lambda_f, \phi_f, k_f^\alpha, S_f^\alpha$
- Matrix rocktype (m):  $\Lambda_m, \phi_m, k_m^\alpha, S_m^\alpha$

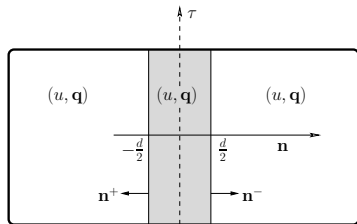


# Dimensional Hybridizing (codimension 1 in the fracture)

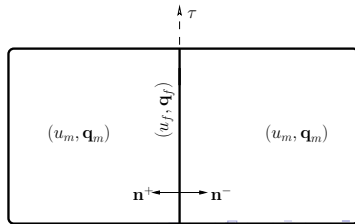
[Granet et al 2001], [Jaffré et al. 2002], [Bogdanov et al 2003], [Faille et al 2003], [Karimi Fard 2004], [Jaffré et al. 2005]

- **Dimensional hybridizing**: averaging the model equations over the fracture width
- **Objectives**: facilitate the mesh generation and lower the number of degrees of freedom

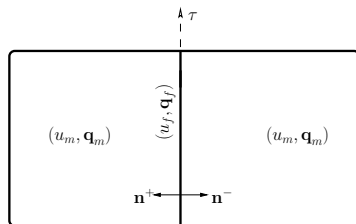
equi-dimensional model:



hybrid-dimensional model:

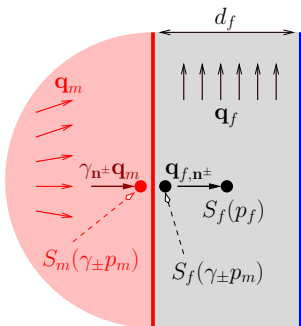


# Hybrid dimensional models



$$\left\{ \begin{array}{l}
 \text{Matrix Darcy Law: } \mathbf{q}_m^\alpha = -k_m^\alpha(S_m^\alpha(p_m)) \Lambda_m(\nabla u_m^\alpha - \rho^\alpha \mathbf{g}) \\
 \text{Matrix Vol. Cons.: } \phi_m \partial_t S_m^\alpha(p_m) + \text{div}(\mathbf{q}_m^\alpha) = 0 \\
 \text{Fracture Darcy Law: } \mathbf{q}_f^\alpha = -d_f k_f^\alpha(S_f^\alpha(p_f)) \Lambda_{f,\tau}(\nabla_\tau u_f^\alpha - \rho^\alpha \mathbf{g}_\tau) \\
 \text{Fracture Vol. Cons.: } \phi_f d_f \partial_t S_f^\alpha(p_f) + \text{div}_\tau(\mathbf{q}_f^\alpha) + \gamma_{n^+} \mathbf{q}_m^\alpha + \gamma_{n^-} \mathbf{q}_m^\alpha = 0
 \end{array} \right.$$

# Transmission conditions at the matrix fracture interface



## ■ Discontinuous pressure model:

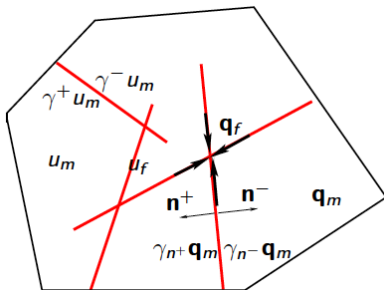
$$\gamma_{n^\pm} \mathbf{q}_m^\alpha = \mathbf{q}_{f,n^\pm}^\alpha \approx$$

$$k_f^\alpha (S_f^\alpha(\gamma \pm p_m)) \Lambda_{f,n} \left( \frac{\gamma \pm u_m^\alpha - u_f^\alpha}{\frac{d_f}{2}} - \rho^\alpha \mathbf{g} \cdot \mathbf{n}^\pm \right)^+ \\ + k_f^\alpha (S_f^\alpha(p_f)) \Lambda_{f,n} \left( \frac{\gamma \pm u_m^\alpha - u_f^\alpha}{\frac{d_f}{2}} - \rho^\alpha \mathbf{g} \cdot \mathbf{n}^\pm \right)^-$$

## ■ Continuous pressure model $\left( \frac{\Lambda_{f,n}}{d_f} \gg \frac{\Lambda_{m,n}}{L} \right)$ :

$$\gamma_+ u_m^\alpha = \gamma_- u_m^\alpha = u_f^\alpha.$$

# Generalization to complex Discrete Fracture Network



- Pressure continuity and flux conservation is assumed at fracture intersections
- Zero flux is assumed at immersed fracture tips

# The Vertex Approximate Gradient Discretization (VAG)

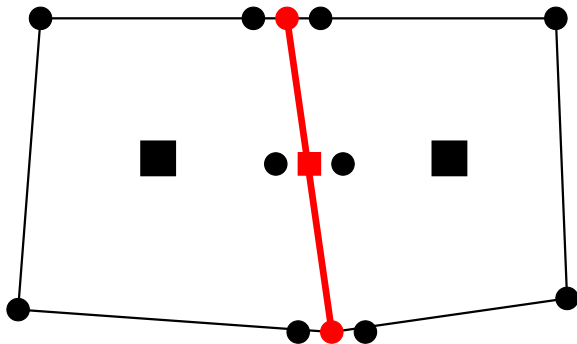
# Discretization: state of the art

- MFE or MHFE: Jaffré et al 2002, Firoozabadi 2008
- TPFA: Faille et al. 2003, Karimi-Fard et al 2004
- CVFE: Bogdanov et al. 2003, Bastian et al 2006, Firoozabadi et al 2007
- XFEM type methods: Formaggia, Scotti et al 2012
- MPFA: Faille et al, Nordbotten et al, 2012, Edwards 2014
- HFV, MFD: Faille et al, Formaggia et al 2016
- ...

## Our contributions:

- For both continuous and discontinuous of models
  - Extension of the Gradient scheme framework (Eymard et al 2010)
  - VAG and HFV discretizations
  - Two phase flows

# VAG scheme: degrees of Freedom (discontinuous pressure model)



- Two matrix cells touching a fracture face
  - Matrix d.o.f. (black)
  - Fracture d.o.f. (red)

# VAG Matrix-Matrix and Fracture-Fracture Fluxes

## ■ mm (ff) fluxes:

- upwind (w.r.t. the phase mobility)
- MPFA
- local stencil to each cell  $K$   
(fracture face  $\sigma$ )

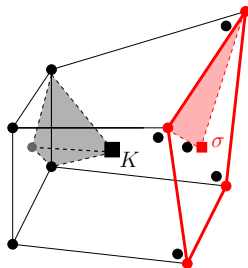
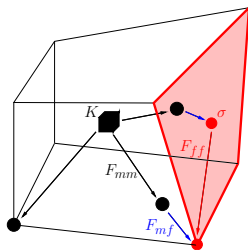
$$F_{K\nu}(u) = k_m(S_m(p_K))f_{K\nu}(u)^+ + k_m(S_m(p_\nu))f_{K\nu}(u)^-$$

$$f_{K\nu}(u) = \sum_{\nu' \in \partial K} T_K^{\nu\nu'} (u_K - u_{\nu'} - \rho(\mathbf{x}_K - \mathbf{x}_{\nu'}) \cdot \mathbf{g})$$

## ■ mm (ff) transmissivities:

- conforming  $P^1$  FE gradient on a tetrahedral (triangular) submesh ( $\{\mathbf{e}_\nu\}_\nu = P^1$  FE Basis Functions)

$$T_K^{\nu\nu'} = \int_K \Lambda \nabla \mathbf{e}_\nu \nabla \mathbf{e}_{\nu'} dx$$



# VAG Matrix-Fracture Fluxes

## mf fluxes:

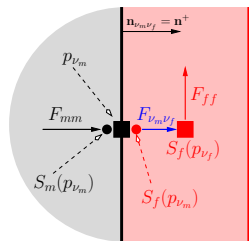
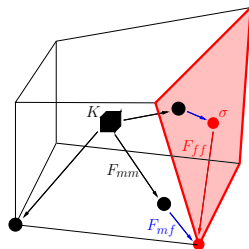
- upwind (w.r.t. the phase mobility)
- TPFA
- Saturation jump at mf interfaces
- Gravity in normal direction

$$F_{\nu_m \nu_f}(u) = k_f(S_f(p_{\nu_m}))f_{\nu_m \nu_f}(u)^+ + k_f(S_f(p_{\nu_f}))f_{\nu_m \nu_f}(u)^-$$

$$f_{\nu_m \nu_f}(u) = T_{\nu_m \nu_f}(u_{\nu_m} - u_{\nu_f} - \frac{\rho d_f}{2} \mathbf{g} \cdot \mathbf{n}_{\nu_m \nu_f})$$

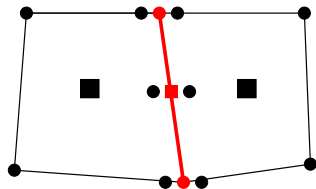
## mf transmissivities:

- Mass Lumping of P<sup>1</sup> FE basis function traces

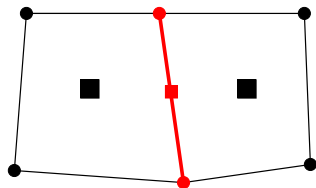


# Hybrid Continuous Pressure and Hybrid Discontinuous Pressure degrees of freedom

- Hybrid Discontinuous Pressure



- Hybrid Continuous Pressure



# Hybrid Continuous Pressure model: Fluxes

## Matrix mm fluxes

$$F_{K\nu}(u) = k_m(S_m(p_K))f_{K\nu}(u)^+ + k_m(S_m(p_\nu))f_{K\nu}(u)^-$$

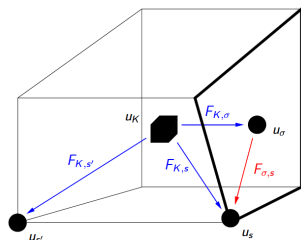
$$f_{K\nu}(u) = \sum_{\nu' \in \partial K} T_K^{\nu\nu'} (u_K - u_{\nu'} - \rho(\mathbf{x}_K - \mathbf{x}_{\nu'}) \cdot \mathbf{g})$$

## Fracture ff fluxes

$$F_{\sigma s}(u) = k_f(S_f(p_\sigma))f_{\sigma s}(u)^+ + k_f(S_f(p_s))f_{\sigma s}(u)^-$$

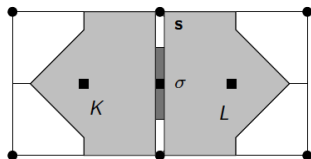
$$f_{\sigma s}(u) = \sum_{s' \in \partial\sigma} T_\sigma^{ss'} (u_\sigma - u_{s'} - \rho(\mathbf{x}_\sigma - \mathbf{x}_{s'}) \cdot \mathbf{g})$$

## No mf fluxes

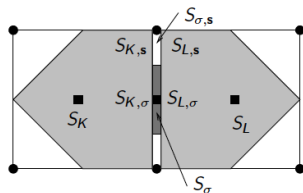


# Hybrid Continuous Pressure model

## Control Volumes



## Saturations at matrix fracture interfaces



$$\left\{ \begin{array}{l} S_{K,\nu}^\alpha = S_m^\alpha(p_\nu), \\ S_K^\alpha = S_m^\alpha(p_K), \end{array} \right. \quad \left\{ \begin{array}{l} S_{\sigma,s}^\alpha = S_f^\alpha(p_s), \\ S_\sigma^\alpha = S_f^\alpha(p_\sigma). \end{array} \right.$$

# Applications and Numerical Results

# Comparison of equi- and hybrid-dimensional models: with J. Hennicker, K. Brenner and P. Samier

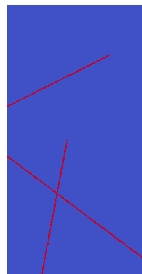
- $\Omega = (0, 400) \times (0, 800)$  m
- Equi-dimensional mesh: 22500 triangles
- Hybrid dimensional mesh: 16900 triangles
- **Matrix:**

$$\phi_m = 0.2, \quad \Lambda_m \text{ isotropic}$$

- **Faults:**

$$d_f = 4m, \quad \phi_f = 0.4, \quad \Lambda_f \text{ isotropic}$$

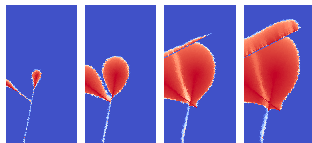
- Injection of oil in the bottom fault
- Initially saturated with water



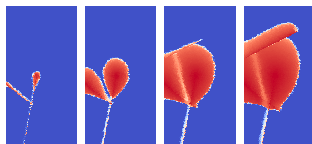
Drains:  $\Lambda_f/\Lambda_m = 1000$ ;  $p_{c,m}(S_m^o) = p_{c,f}(S_f^o) = 0$

**Zero Capillary Pressure:**  $p_{c,m}(S_m^o) = p_{c,f}(S_f^o) = 0$

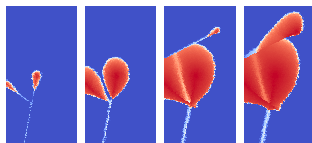
■ Equi dim



■ Hybrid Disc.



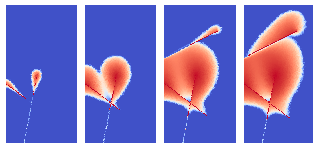
■ Hybrid Cont.



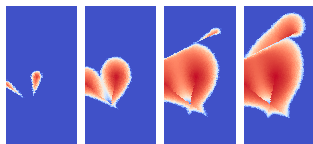
Drains:  $\Lambda_f/\Lambda_m = 1000$ ;  $p_{c,m} \neq 0$ ;  $p_{c,f} = 0$

**Capillary Pressure:**  $p_{c,m}(S_m^o) = -10^5 \ln(S_m^o)$ ;  $p_{c,f} = 0$

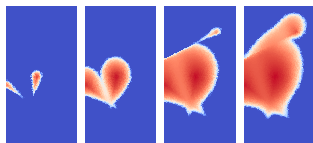
■ Equi dim



■ Hybrid Disc.

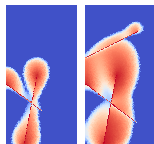


■ Hybrid Cont.

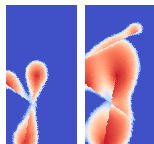


Drains:  $\Lambda_f/\Lambda_m = 100$ ;  $p_{c,m} = -10^5 \ln(S_m^o)$ ,  
 $p_{c,f} = -10^4 \ln(S_m^o)$

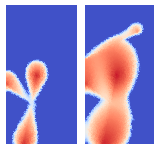
■ Equi dim



■ Hybrid Disc.



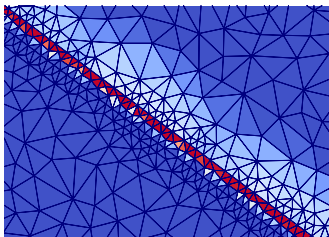
■ Hybrid Cont.



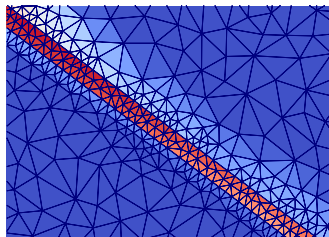
Drains:  $\Lambda_f/\Lambda_m = 100$ ;  $p_{c,m} = -10^5 \ln(S_m^o)$

Equi-Dimensional Model: Saturation Stratification in the fault Network

$$p_{c,f} = 0$$



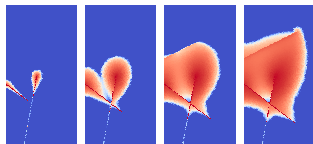
$$p_{c,f} = -10^4 \ln(S_m^o)$$



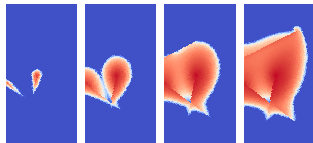
Drain-Barrier:  $\Lambda_f^{drain} / \Lambda_m = 1000$ ;  $\Lambda_f^{barrier} / \Lambda_m = 0.01$

**Capillary Pressure:**  $p_{c,m} = -10^5 \ln(S_m^o)$ ;  $p_{c,f} = 0$

■ Equi dim

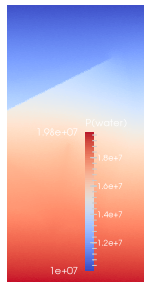


■ Hybrid Disc.

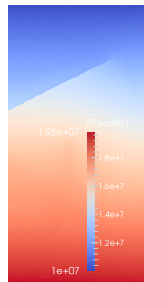


Drain-Barrier:  $\Lambda_f^{drain} / \Lambda_m = 1000$ ;  $\Lambda_f^{barrier} / \Lambda_m = 0.01$

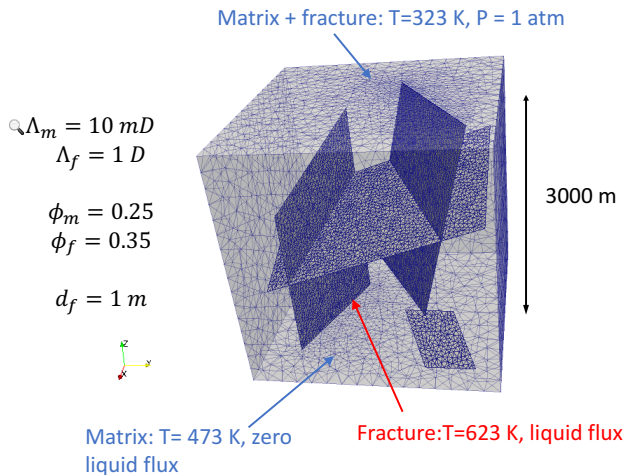
Equi dim.



Hybrid Disc.



# High energy geothermal test case: with F. Xing and S. Lopez (BRGM)



# Thermal two phase flow

**Model:**  $H_2O$  component in liquid or vapor phase

**Unknowns:**  $P, T, S^l, S^g$

**Continuous Pressure model**

$P, T, S$  formulation.

Conservation of mass, energy and volume:

$$\begin{cases} \phi \partial_t \left( \sum_{\alpha=l,g} \rho^\alpha S^\alpha \right) + \operatorname{div} \left( \sum_{\alpha=l,g} \rho^\alpha \mathbf{q}^\alpha \right) = 0, \\ \phi \partial_t \left( \sum_{\alpha=l,g} \rho^\alpha e^\alpha S^\alpha \right) + (1 - \phi) \partial_t E_r + \operatorname{div} \left( \sum_{\alpha=l,g} \rho^\alpha h^\alpha \mathbf{q}^\alpha - \lambda \nabla T \right) = 0, \\ S^l + S^g = 0, \end{cases}$$

+ liquid vapor thermodynamical equilibrium:

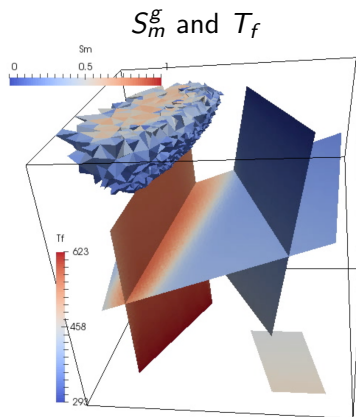
$$\begin{cases} T = T_{sat}(P) & \text{if } S^g > 0 \text{ and } S^l > 0, \\ S^g = 0 & \text{if } T < T_{sat}(P), \\ S^l = 0 & \text{if } T > T_{sat}(P). \end{cases}$$

# High energy geothermy: temperature and gas saturation

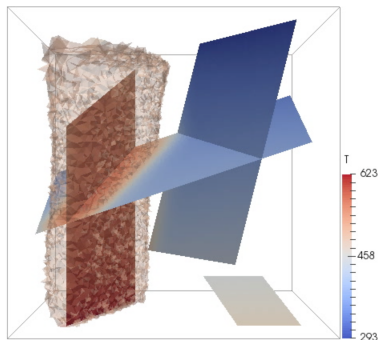
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# High energy geothermy: temperature and gas saturation



$T_f$  and  $T_m > 500$  K



# Conclusion and Perspectives

- Two phase hybrid dimensional model taking into account
  - networks of fractures
  - drains and barriers
  - discontinuous capillary pressures
  - gravity
  
- On going work
  - Convergence analysis using the gradient scheme framework (with J. Droniou)
  - Geothermal systems: ANR project with BRGM, Storengy, MdS, LJLL, LJAD
  - Large networks

# Acknowledgements

Thanks for your attention and to Total, Engie and BRGM for their support.

